Summary of shock-induced polymorphic phase transition observations

FABLE AI.

tions to dense phases could possibly explain the anomalously low compressibility in the mixed phase region above 14.4 GPa. Other materials such as Al_2O_3 have been observed to display yield behavior similar to quartz, and geologic materials are possible candidates for similar behavior. The question of heterogeneous melting and its effect on subsequent high-pressure loading in quartz is a problem of importance that should be pursued with some urgency.

As the different experimental investigations have been summarized, the role of experimental technique has been found to be significant. Better understanding of the bismuth transition involved the use of projectile impact loading techniques and the use of detectors with capabilities for accurate time-resolved sample response measurements. A similar situation is noted for the iron transition. The combination of projectile impact loading and time-resolved measurements appears to be particularly effective for studying shock-induced phase transitions.

Finally, it is perhaps worthwhile to emphasize again that it is a mistake to overgeneralize concerning any aspect of shock-induced phase transitions in either a positive or negative sense. There are many different situations that must be considered on their own merit. It is clear, however, that shock loading experiments can provide credible data concerning pressure-induced transitions. Nevertheless, technique is still critical and it is relatively easy to make errors of interpretation. Comprehensive investigations in the hands of skilled observers, along with critical interpretations of the data, will undoubtedly yield valuable thermodynamic data on phase transitions which may be uniquely obtained under shock loading or may prove to be valuable supplements to static high-pressure data.

Note added in proof : Several references which were inadvertently omitted or have recently come to our attention are the following:

(1) on shock induced vaporization, the paper by Horung and Michel (1972);

(2) on melting in magnesium under shock loading, the paper by Urtieu and Grover (1977);

(3) additional data on transitions in titanium, zirconium, and hafnium are given in McQueen *et al.* (1970);

(4) a thorough study of phase transitions in shock compressed BN is described in Gust and Young (1977); and

(5) the excellent review of optical properties under shock compression by Kormer (1977) summarizes melting curves for alkali halides, and comments upon optical effects associated with polymorphic phase transitions.

ACKNOWLEDGMENT

A Sandia Laboratories internal study group on polymorphic phase transformations, composed of P. C. Lysne, G. A. Samara, L. C. Bartel, and R. A. Graham, provided the initial impetus for the tabular summary of polymorphic phase transformations presented in the Appendix.

APPENDIX A

A summary of polymorphic phase transformations is presented in Table A1.

Material	Condition	Transition Stress (GPa)	Transition conditions GPa) Compression (%)	Technique	Remarks	References
A. Iron and iron alloys	AN A A					11000 B to rotant
Iron						
Armco iron	AR	13.6-13.0	6.69-6.37	E-1	7.2–57 mm	Bancroft et al. (1956)
Armco iron	Ann	13.2-12.5	6.41-6.18	E-1	25–57 mm, +	Minshall (1961)
Armco iron	AR	12.8	6.41	E-1	25 mm	Minshall (1961)
Armco iron	CR	13.5	6.57	E-1	25 mm	Minshall (1961)
Armco iron	Ann	13.6	6.49	E-1	$25 \text{ mm}, T_0 = 222 \text{ K}$	Minshall (1961)
Armco iron	Ann	13.2	6.26	E-1	$25 \text{ mm}, T_0 = 330 \text{ K}$	Minshall (1961)
Armco iron	AR			P-16	Smooth spall	Erkman (1961)
Armco iron	AR	15.0-1.9		D-16	24 T_0 values 78-1158 K, apparent	Johnson et al. (1962)
100 P 100					triple point	
Armco iron	AR	14.5-12.5	6.9-6.2	E .	Prism sample, optical lever	Peyre et al. (1965)
Armco iron	Ann	12.9 ± 0.1	6.4 ± 0.05	E-1	25 mm, \$	Loree et al. (1966a)
Armco iron	AR			E-13	Wave structure, *	Novikov et al. (1965)
Armco iron		15.0		P-11	4–17 mm, +	Anan'in et al. (1973)
Armco iron		14.1-13.1		P-4	1-25 mm	Forbes et al. (1975)
Armco iron	AR	13.7-12.9	6.3	G-9	$3-19 \text{ mm}, +, \psi, \phi, \tau$	Barker et al. (1974)
Electrolytic iron	AR			E-15	Shock demagnetization	Royce (1968)
Iron	AR			E, G-14	Electrical resistance	Wong et al. (1968)
Iron	AR			E-15	Demagnetization eddy currents	Wong (1969)
Iron	and the second s			E-14	Electrical resistance	Fuller et al. (1962)
Iron	AR	Marcher		E-14	Electrical resistance, demagnetization	Keeler et al. (1969)
					eddy currents	

(Continued)

See 12 5		Transition conditions				
erial	Condition	Stress (GPa)	Compression (%)	Technique	Remarks	References
ued)			1	A L CAR	apparent here an	BOLD I TURN
	AR	The state of the second	· · · · · · · · · · · · · · · · · · ·	P-20	Double shock and rarefaction shock	Balchan (1963)
	Powder/Bakelite mixture	9.4-11		E	Shock demagnetization; $\rho_0 = 5.33 \text{ Mg/m}^3$	Novikov et al. (1974
					, , , , , , , , , , , , , , , , , , ,	normor et ut. (101-
teels						
	Ann	•••	•••	P-16	Smooth spall for $P > 14.0$ GPa, ASTM	Banks (1968)
					grain size 2–3	the second second second
el	AR	12.9	6.2	E-1	51 mm	Minshall (1961)
el	Ann	13.7-12.8	6.7-6.2	E-1	27-51 mm	Minshall (1961)
eel	Hot rolled			E-2	Wedge sample, qualitative	Katz et al. (1959)
el	Ann	13.6	6.6	E-1	27 mm	Minshall (1961)
el	Ann •••	14.1	6.7	E-1	27 mm	Minshall (1961)
teel		15.3		P-11	6-20 mm, +	Anan'in et al. (1973
on)	17			1000	Ales unles line	
steel	AR	16.0	***	P-11	Also unloading	Anan'in et al. (1973
on)	DCCO CO	10.0	and an other	D 11	Also unloading	A
steel	RC60-62	16.2	A CONTRACTOR OF THE OWNER OF THE	P-11	Also unloading	Anan'in et al. (1973
on)						
lloys						
Ni	AR	12.0		E-1	$\rho_0 = 7.848 \text{ Mg/m}^3$	Fowler <i>et al</i> . (1961)
Ni	AR	11.8	- in the second of	E-1	$\rho_0 = 7.855 \text{ Mg/m}^3$	Fowler <i>et al.</i> (1961)
6 Ni	1273 K, 1 h	12.1	6.75	E-4	$\rho_0 = 7.892 \text{ Mg/m}^3, 6.4 \text{ mm}$	Gust <i>et al.</i> (1970)
6 Ni	AR	11.0		E-1	$\rho_0 = 7.878 \text{ Mg/m}^3$	Fowler <i>et al.</i> (1961)
Ni	AR	10.2		E-1	$\rho_0 = 7.910 \text{ Mg/m}^3$	Fowler <i>et al.</i> (1961)
Ni	AR	11.7		E-1		Fowler <i>et al</i> . (1961)
Ni	AR	8.5	4.2	E-1	•••	Loree et al. (1966a)
Ni	AR	8.0		E-1		Loree et al. (1966a)
Ni	AR	5.5	3.4	E-1	8	Loree et al. (1966a)
% Ni	Ann, quench	7.0-<1.0	4.1-1.2	G-8, 12	$\rho_0 = 8.032 \text{ Mg/m}^3$, 7 mm, 9 various	Rohde (1970)
王羽	liquid N 168 h				T_0 values between 298 and 663 K, γ phase recovered	
% Ni	Ann, quench			G-8, 16	Partial transformation at 2.0 GPa	Rohde <i>et al.</i> (1968)
	liquid N 168 h			u=0, 10	r ar that it ansist mation at 2.0 Gra	Ronde et at. (1968)
the state of the	Inquita IV 100 H					
m alloys					是 不是 的 医 路 田 田 田 田 田 田 田 田	
r	AR	12.8		E-1	$\rho_0 = 7.825 \text{ Mg/m}^3$	Fowler <i>et al</i> . (1961)
Cr	AR	12.6	1 C	E-1	$\rho_0 = 7.793 \text{ Mg/m}^3$	Fowler <i>et al</i> . (1961)
Cr	AR	12.5	1 · · · · · · ·	E-1	B. B	Fowler <i>et al</i> . (1961)
6 Cr	AR	13.3	1 3.4 8 6 8	E-1	$\rho_0 = 7.747 \text{ Mg/m}^3$	Fowler <i>et al</i> . (1961)
Cr	AR	14.9	1	E-1	山田田田田田田田田田田田田田	Fowler <i>et al</i> . (1961)
Cr	AR	18.2		E-1	E*** 1 2 0	Fowler <i>et al</i> . (1961)
Cr	1273 K, 1 h,	13.4-13.1	6.40-6.10	E-4	$p_0 = 7.757 \text{ Mg/m}^3, 6.4 \text{ mm}$	Gust et al. (1970)
	water quench				Share and a grade the short	
Cr	1273 K, 1 h,	15.7-15.4	7.60-7.44	E-4	$\rho_0 = 7.724 \text{ Mg/m}^3, 6.4 \text{ mm}$	Gust et al. (1970)
R HA	water quench				I TEACOR STREET	
Cr	1273 K, 1 h,	20.7	9.19	E-4	$ \rho_0 = 7.644 \text{ Mg/m}^3, 6.4 \text{ mm} $	Gust et al. (1970)
1 5 1 4	water quench					
Cr	1273 K, 1 h,	23.8-22.3	10.5-9.83	E-4	$\rho_0 = 7.618 \text{ Mg/m}^3, 6.4 \text{ mm}$	Gust et al. (1970)
E S A	water quench					
se alloys						
Mn	AR	12.4	6.1	E-1		Loree et al. (1966b)
Mn	AR	11.0	5.3	E-1	日本 るい うち きまた うちまたち	Loree et al. (1966b)
	AR	8.5	3.8	E-1	A BERGERERE BALLER	Loree et al. (1966b)
% Mn Mn	AR	5.8-5.3	0.0	Det		LUICE Et at. (10000)